



ATTACHMENT C

Amendments to the Claims

This listing of claims will replace all prior versions, and listings, of claims in the application.

1. (currently amended) A reciprocating engine used operating between a minimum speed of rotation Nmin and a maximum speed Nmax comprising; which comprises

a turbocharging unit (2) dimensioned so as to function autonomously when which:

- it supplies the an intake manifold (8) of the engine with compressed air via a cooler;
- it is supplied with gas by the an exhaust manifold (9, CR and CT) of the engine at the exhaust temperature; and
- has a the turbine supply inlet pressure (P3) is substantially equal to the a compressor discharge pressure (P2);

in such a way that at constant air temperature and with a fixed geometry, the turbocharging unit delivers a substantially constant volume of cooled air Vc when the compressor discharge pressure varies,

and that the volume Vc is substantially proportional to the a turbine inlet section Sd offered to the hot gases,

wherein the turbine inlet pressure (P3) is maintained substantially equal to the compressor discharge pressure (P2) by a EGR bypass (3) provided between the intake manifold (8) and the an exhaust manifold (9) dimensioned so as to transfer the a flow of exhaust gas to the intake manifold without significant loss of pressure,

and wherein the volume of air Vc is less than the volume drawn in by the engine at the speed Nmax in such a way that a flow of hot gases is drawn in again by the engine via the EGR bypass (3) above the speed Na, known as the a turbocharging adaptation speed Na, where the volume drawn in is equal to volume Vc, and a flow of air is deflected towards the turbine below the adaptation speed Na.

2. (currently amended) A reciprocating engine as claimed in Claim 1, wherein the EGR bypass (3) has an EGR valve (6) making it possible to increase the turbine inlet pressure above the compressor discharge pressure.

3. (currently amended) A reciprocating engine as claimed in Claim 1, wherein the turbocharging unit has an intake valve (7) situated on ~~the~~a compressed air discharge conduit ~~making it possible to increase the compressor~~ discharge pressure above the turbine inlet pressure.

4. (currently amended) A reciprocating engine as claimed in Claim 1, wherein the EGR bypass conduit (3) has a gas cooler (4) at ~~an~~ adjustable temperature, preferably adjustable to cool gas up to a temperature close to that of the fresh air.

5. (currently amended) A reciprocating engine as claimed in Claim 4, wherein the adjustment of the temperature is effected by controlling a bypass of the cooler.

6. (currently amended) A method of supplying an reciprocating engine as claimed in Claim 4, wherein the EGR bypass temperature is controlled to create the desired excess of air for the combustion in the engine.

7. (currently amended) A method of supplying a reciprocating engine as claimed in Claim 4, wherein the EGR bypass temperature is controlled so that ~~the~~a mass of the recycled gases remains substantially equal to ~~the~~a mass of the fresh air up to the speed at which this temperature returns to the exhaust temperature, the recycled mass becoming greater than the mass of the fresh air above this speed.

8. (currently amended) A method of supplying a reciprocating engine as claimed in Claim 5, wherein the gas cooler is totally bypassed when the engine does not deliver propulsive power.

9. (currently amended) A method of supplying a reciprocating engine as claimed in Claim 8, wherein for cold starting and operating at idling speed, ~~the~~an adjustment of the turbine valves (6) and (7) and/or ~~the~~a timing of the engine valves is adjusted so that the excess of combustion air is minimal for ~~the~~a desired level of depollution.

10. (currently amended) A reciprocating engine as claimed in Claim 1, wherein:
the adaptation speed N_a is substantially equal to $N_{min}/2$ so that ~~the-a~~ volume of
recycled gases is at least equal to that of the fresh air, and
the minimum temperature of the recycled gases is preferably close to the
temperature of the fresh air so that ~~the-a~~ mass of the recycled gases is at least equal to
that of the fresh air at the minimum speed used N_{min} in order to depollute during all the
ranges of use of the engine.
11. (currently amended) A reciprocating engine as claimed in Claim 4, wherein:
the adaptation speed N_a is substantially equal to $N_{min}/2$ so that the volume of
recycled gases is at least equal to that of the fresh air, and
the minimum temperature of the recycled gases is preferably close to the
temperature of the fresh air so that ~~the-a~~ mass of the recycled gases is at least equal to
that of the fresh air at the minimum speed used N_{min} in order to depollute during all the
ranges of use of the engine.
12. (currently amended) A reciprocating engine as claimed in Claim 1,
wherein the turbocharging unit has a low-pressure LP turbocharger and a high-
pressure HP turbocharger, ~~of which the compressors of which~~ work in series with,
preferably, a cooling of the air between the compressors and ~~the-an~~ exhaust outlet
section S_d ~~can be adjusted which is adjustable~~ between a minimum S_d min and a
maximum S_d max by one or a combination of the following means:
- adjustment of ~~the-a~~ variable section of ~~the-a~~ gas distributor of the turbines,
- opening of a bypass between ~~the-an~~ inlet and ~~the-an~~ outlet of the turbines,
- passage from a series configuration to a parallel configuration of the turbines,
the turbocharging adaptation speed N_a thus ~~becoming being~~ adjustable, in a continuous
or discontinuous manner, between two values N_a min and N_a max. In the following, a
~~bypass between the inlet and the outlet of a turbine will be called a waste gate.~~

13. (currently amended) A reciprocating engine as claimed in Claim 12, wherein the minimum outlet section Sd min offered to the gases is formed by the two turbines mounted in series at maximum closure ~~if their distributor is variable and all waste gates are closed if they exist.~~

14. (currently amended) A reciprocating engine as claimed in Claim 13, which operates on a 4-stroke cycle with a fixed timing of ~~the associated~~ valves.

15. (currently amended) A reciprocating engine as claimed in Claim 14, wherein the maximum outlet section Sd max offered to the gases is formed by the two turbines with which have fixed distributors mounted in parallel, and wherein, in order to pass the turbines from the series configuration to the parallel configuration, the following manoeuvres ~~to be~~ carried out successively:

- progressive partial opening of an ~~the~~ HP waste gate between the inlet and the outlet of a turbine,
- progressive and simultaneous partial opening of the HP and an LP waste gates
- simultaneously and rapidly: total opening of the HP waste gate, total closure of the LP waste gate, putting the outlet of the HP turbine into communication with the outlet of the LP turbine.

16. (currently amended) A reciprocating engine as claimed in Claim 14, wherein the maximum outlet section Sd max offered to the gases is formed by a LP turbine with fixed distributor and a HP turbine with variable distributor mounted in parallel, the HP distributor being fully open, and wherein, in order to pass the turbines from the series configuration to the parallel configuration, the following manoeuvres to be carried out successively:

- progressive opening of ~~the~~ a distributor of the HP turbine,
- progressive partial opening of ~~the~~ an LP waste gate,
- simultaneously and rapidly: total opening of the LP waste gate and putting the outlet of the HP turbine into communication with the outlet of the LP turbine.

17. (currently amended) A method of supplying an reciprocating engine as claimed in Claim 2,

wherein, in order to limit the-a frequency of changing the-a configuration, the geometry is immobilised~~immobilized~~ for a type of driving which implements a limited power range, ~~for example the series configuration of the turbines for driving in town and the parallel configuration for driving on the open road, and the power thresholds corresponding to each configuration can be~~ crossed for manoeuvres of short duration, such as accelerating, overtaking, bursts of speed, etc., and

wherein the power thresholds may be crossed as follows:

- by closure of the EGR valve if the pressure in the exhaust manifold can be increased,

- by opening of one or two waste gates if the exhaust temperature can be increased,

by closure of the an intake valve if the maximum cycle pressure is reached or if the compressors are close to their maximum flow rate.

18. (currently amended) A method of supplying an reciprocating engine as claimed in Claim 3,

wherein, in order to limit the-a frequency of changing the-a configuration, the geometry is immobilised~~immobilized~~ for a type of driving which implements a limited power range, ~~for example the series configuration for driving in town and the parallel configuration for driving on the open road, and the power thresholds corresponding to each configuration can be~~ crossed for manoeuvres of short duration, such as accelerating, overtaking, bursts of speed, etc., and

wherein the thresholds may be crossed as follows:

- by closure of the an EGR valve if the pressure in the exhaust manifold can be increased,

- by opening of one or two waste gates if the exhaust temperature can be increased,

- by closure of the an intake valve if the maximum cycle pressure is reached or if the compressors are close to their maximum flow rate.

19. (currently amended) A method of supplying an reciprocating engine as claimed in Claim 12,

wherein, in order to limit the-a frequency of changing the-a configuration, the geometry is immobilised~~immobilized~~ for a type of driving which implements a limited power range, for example the series configuration for driving in town and the parallel configuration for driving on the open road, and the power thresholds corresponding to each configuration can be~~are~~ crossed for manoeuvres of short duration, such as accelerating, overtaking, bursts of speed, etc., and

wherein the thresholds may be crossed as follows:

- by closure of the EGR valve if the pressure in the exhaust manifold can be increased,

- by opening of one or two waste gates if the exhaust temperature can be increased,

- by closure of the ~~an~~ intake valve if the maximum cycle pressure is reached or if the compressors are close to their maximum flow rate.

20. (currently amended) A reciprocating engine as claimed in Claim 15, wherein the LP waste gate has a second seat in order simultaneously to effect the-a closure of the LP turbine inlet/outlet bypass and putting the HP turbine outlet into communication with the LP turbine outlet.

21. (currently amended) A reciprocating engine as claimed in Claim 15, wherein the two waste gates are concentric and have stops in such a way that their simultaneous movements thereof are actuated by one of them and communicated to the other by the said stops.

22. (currently amended) A reciprocating engine as claimed in Claim 14, wherein the maximum outlet section Sd max is formed by two turbines with fully open variable distributors mounted in series, and wherein the distributors are opened simultaneously

in order to maintain the intake pressure at its-a maximum desired value thereof on the-a full load curve.

23. (currently amended) A reciprocating engine as claimed in Claim 13,
wherein the-a timing of the-valves can beis controlled so-as-to displace the-a closure of the-an associated cylinder between the vicinity of the BDC and the mid-stroke of the-an associated piston,

wherein the maximum outlet section Sd is formed by the HP turbine in series configuration with the distributor fully open if it is variable, the HP waste gate fully open in the contrary case; and

wherein the turbines are dimensioned so-as-to permit the compressors thereof to reach their maximum pressure ratios thereof simultaneously.

24. (currently amended) A method of supplying an reciprocating engine as claimed in Claim 23, wherein the-a full load curve as a function of the speed is as follows:

from Nmin to 2 Nmin, the-an intake closure FA passes from the BDC (bottom dead centre) to approximately 90 degrees of the-a crankshaft after the BDC in such a way as to maintain the-a cycle pressure below its-a desired value thereof, and

the-a distributor or the-an HP waste gate is closed;

from 2 Nmin to approximately 3 Nmin, the HP distributor or the HP waste gate is open and possibly the LP waste gate in order to maintain the-an intake pressure at its-a maximum desired value thereof, and

the intake closure FA is maintained at 90 degrees of the crankshaft after the BDC; and

from 3 Nmin to Nmax, the-a global flow rate of fuel is kept constant in order to maintain the intake pressure at its-a limiting value thereof, and

at partial load, the-a timing of intake closure FA will be-is controlled according to a map memorised by-store in the-an engine control computer.

25. (currently amended) A reciprocating engine as claimed in Claim 13, which operates on the 2-stroke cycle, and wherein:

~~the intake ports are closed by valves,~~

~~the exhaust ports are closed by valves and communicate with one single exhaust manifold,~~

~~the an external recycling phase precedes the scavenging,~~

~~the a timing of the valves can beis controlled so as to displace the a closure of the an associated cylinder between the vicinity of the BDC and the mid-stroke of the an associated piston,~~

~~the a maximum outlet section Sd is formed by the HP turbine in series configuration with the distributor fully open if it is variable, the HP waste gate fully open in the contrary case,~~

~~the turbines are dimensioned so as to permit the associated compressors to reach their maximum pressure ratios thereof simultaneously, and~~

~~the EGR valve bypass is replaced by one of a check valve or a closable aerodynamic diode.~~

26. (currently amended) A method of supplying an reciprocating engine as claimed in Claim 25, wherein the a full load curve as a function of the speed is as follows:

- from Nmin to 2 Nmin, the closure of the cylinder passes from the BDC to approximately 90 degrees of the crankshaft after the BDC in such a way as to maintain the cycle pressure at its a desired value thereof,

- the a distributor or the an HP waste gate is closed,

- from 2 Nmin to approximately 3 Nmin, the HP distributor or the HP waste gate is open and possibly the LP waste gate in order to maintain the an intake pressure at its a maximum desired value thereof,

- an intake closure FA is maintained at 90 degrees of the crankshaft after the BDC,

- from 3 Nmin to Nmax, the a global flow rate of fuel is kept constant in order to maintain the intake pressure at its a limiting value thereof; and

wherein, in order to maximise maximize the cooled external EGR, the depolluted partial loads can beare effected as follows:

- the cylinder remains closed in the vicinity of the BDC and the turbines remain in closed configuration up to the compressor discharge pressure P2-limit for this timing,
- the turbines are then opened in order to maintain the compressor discharge pressure P2 at its-a limiting value thereof,
- the aerodynamic diode is used when the external recycling flow stops.

27. (currently amended) A reciprocating engine as claimed in Claim 13, which operates on the 2-stroke cycle, it has

wherein there are two exhaust ports per cylinder, closed by valves, which communicate respectively with an exhaust manifold connected to the turbine and an exhaust manifold connected to the EGR conduit bypass and/or to the turbine via a controlled distributor valve,

wherein the timing of the valve assigned to the EGR bypass can be is controlled so-as-to displace the closure of the cylinder between the vicinity of the BDC and the mid-stroke of the an associated piston, wherein:

the an external recycling phase precedes the scavenging when the cylinder closes in the vicinity of the BDC and follows itthe scavenging when the cylinder closes at the mid-stroke of the piston;

the maximum outlet section Sd is formed by the HP turbine in series configuration with the distributor fully open if it is variable, the HP waste gate fully open in the contrary case.;

the turbines are dimensioned so-as-to permit the compressors to reach their maximum pressure ratios thereof simultaneously; and

the EGR valve bypass is replaced by one of a check valve or a closable aerodynamic diode.

28. (currently amended) A method of supplying an reciprocating engine as claimed in Claim 27, wherein:

the compressor discharge pressure P2-is lower than the-a limit allowed for theis timing,

the distributor valve is in the-a recycling position,

the cylinder is closed in the vicinity of the BDC,
the a distributor or the an HP waste gate are is closed,
when the pressure reaches the limiting value allowed for this timing, the closure
of the cylinder is displaced to the mid-stroke of the piston in order substantially to
double the allowed compressor discharge pressure P2-limit,
the distributor valve remains in the recycling position,
the distributor or the HP waste gate remains closed,
the compressor discharge pressure P2-reaches the-a new limit allowed for this
new timing,
the distributor valve blocks the recycling,
the distributor or the HP waste gate opens in order to keep the compressor
discharge pressure P2-at its-a new allowed limit thereof, and
the transition can beis made by one of progressively in the two directions or
rapidly with a hysteresis.

29. (currently amended) A method of supplying a reciprocating engine as claimed in
Claim 6, wherein:

at full load the variable geometry is controlled so-as-to maintain a parameter at its
a limiting desired value thereof;
at partial load the variable geometry is controlled so-as-to optimise~~optimize~~ the
depollution and/or the performance according to a map memorised~~stored~~ in the-an
engine control computer.

30. (currently amended) A method of supplying a reciprocating engine as claimed in
Claim 7, wherein:

at full load the variable geometry is controlled so-as-to maintain a parameter at its
a limiting desired value thereof;
at partial load the variable geometry is controlled so-as-to optimise~~optimize~~ the
depollution and/or the performance according to a map memorised~~stored~~ in the-an
engine control computer.

31. (currently amended) A method of supplying a reciprocating engine as claimed in Claim 8, wherein:

at full load the variable geometry is controlled so as to maintain a parameter at its a limiting desired value thereof;

at partial load the variable geometry is controlled ~~so as to optimiseoptimize~~ the depollution and/or the performance according to a map ~~memorisedstored~~ in the ~~an~~ engine control computer.

32. (currently amended) A method of supplying a reciprocating engine as claimed in Claim 9, wherein:

at full load the variable geometry is controlled so as to maintain a parameter at its a limiting desired value thereof;

at partial load the variable geometry is controlled ~~so as to optimiseoptimize~~ the depollution and/or the performance according to a map ~~memorisedstored~~ in the ~~an~~ engine control computer.

33. (currently amended) A method of supplying a reciprocating engine as claimed in Claim 17, wherein:

at full load the variable geometry is controlled so as to maintain a parameter at its a limiting desired value thereof;

at partial load the variable geometry is controlled ~~so as to optimiseoptimize~~ the depollution and/or the performance according to a map ~~memorisedstored~~ in the ~~an~~ engine control computer.

34. (currently amended) A method of supplying a reciprocating engine as claimed in Claim 18, wherein:

at full load the variable geometry is controlled so as to maintain a parameter at its a limiting desired value thereof;

at partial load the variable geometry is controlled so as to ~~optimiseoptimize~~ the depollution and/or the performance according to a map ~~memorisedstored~~ in the ~~an~~ engine control computer.

35. (currently amended) A method of supplying a reciprocating engine as claimed in Claim 19, wherein:

at full load the variable geometry is controlled so-as-to maintain a parameter at its a limiting desired value thereof;

at partial load the variable geometry is controlled so-as-to optimise~~optimize~~ the depollution and/or the performance according to a map ~~memorised~~stored in the ~~an~~ engine control computer.

36. (currently amended) A method of supplying a reciprocating engine as claimed in Claim 24, wherein:

at full load the variable geometry is controlled so-as-to maintain a parameter at its a limiting desired value thereof;

at partial load the variable geometry is controlled so-as-to optimise~~optimize~~ the depollution and/or the performance according to a map ~~memorised~~stored in the ~~an~~ engine control computer.

37. (currently amended) A method of supplying a reciprocating engine as claimed in Claim 26, wherein:

at full load the variable geometry is controlled so-as-to maintain a parameter at its a limiting desired value thereof;

at partial load the variable geometry is controlled so-as-to optimise~~optimize~~ the depollution and/or the performance according to a map ~~memorised~~stored in the ~~an~~ engine control computer.

38. (currently amended) A method of supplying a reciprocating engine as claimed in Claim 28, wherein:

at full load the variable geometry is controlled so-as-to maintain a parameter at its a limiting desired value thereof;

at partial load the variable geometry is controlled so as to optimise/optimize the depollution and/or the performance according to a map memorised/stored in the an engine control computer.

39. (currently amended) A reciprocating engine as claimed in Claim 1, including a flat cylinder head bearing valves of which the having faces on the a chamber side which are coplanar with the cylinder head and substantially tangent to the a cylinder,

wherein the an intake pipe or pipes terminate(s) by at an oblong nozzle defined by an upper half-cylinder resting on the an upper edge of the a conical seat and tangent to this latter seat along its a generating line thereof situated in a plane substantially perpendicular to the a plane passing through the axis of the seat and through the an axis of the cylinder and through a lower cylinder covering half of the a valve head opposite the said generating line,

wherein the nozzles are also oriented so as to create a tangential speed in the a same direction, and

wherein the angles of the seats are chosen so as to optimise/optimize the stratification of the a combustive charge.

40. (currently amended) A reciprocating engine as claimed in Claim 1, including a flat cylinder head bearing valves of which the having faces on the a chamber side which are coplanar with the cylinder head and substantially tangent to the a cylinder,

wherein the a conical sealing bearing surface of the intake valves is extended towards the a piston by a cylindrical part of having a height slightly greater than the a lift of the said valves,

wherein the conical sealing bearing surfaces seats of the said valves are disposed at the a bottom of cylindrical recesses provided in the a cylinder head in order to receive the said cylindrical parts of the said valves in such a way that the flat lower faces of the valves are in the a plane of the cylinder head when they lower faces rest on

their associated seats thereof, the a clearance between the recesses and the valves being minimal, and

wherein the recesses are provided in the cylinder head which and do not go beyond the following boundaries:

- two cylindrical portions concentric with the-a bore and tangent externally and internally to the cylindrical recess of each valve,

- a conical surface extending the-a half-seat of the valve delimited by a plane passing through the-an axis thereof and the-an axis of the cylinder;

wherein the recesses will are also be oriented so as to create a tangential velocity in the a same direction, and

wherein the-an angle of the seats is chosen so as to optimiseoptimize the-a stratification of the-a combustive charge.

41. (currently amended) A reciprocating engine as Claimed in Claim 39, wherein it includesincluding two diametrically opposed intake valves.

42. (currently amended) A reciprocating engine as Claimed in Claim 40, including wherein it includes two diametrically opposed intake valves.

43. (currently amended) A reciprocating engine as claimed in Claim 1, wherein:
a fraction of the recycled gases is retained in the-a cylinder at the-a closure of the lattercylinder,

the fresh gases are introduced by directive intake conduits with the aim of organisingto create a stratification of the temperatures and the concentrations in the-a chamber at the combustion top dead centre, and

the-a fuel is vaporisedvaporized in the fresh gases.

44. (currently amended) A reciprocating engine as claimed in Claim 43, wherein the fuel is introduced into the pure-fresh air between the compressor and the-an external EGR mixer.

45. (currently amended) A reciprocating engine as claimed in Claim 43, wherein the fuel is introduced into the a mixture between the pure air and the an external EGR.
46. (currently amended) A reciprocating engine as claimed in Claim 43, wherein the an ignition point is controlled by the a timing of the valves at the closure of the cylinder.
47. (currently amended) A reciprocating engine as claimed in Claim 43, wherein the an ignition point is controlled by the a temperature of the an external EGR.
48. (currently amended) A reciprocating engine as claimed in Claim 43, wherein the a first ignition is controlled electrically or is triggered spontaneously by the an injection of the fuel at high pressure at the top dead centre.
49. (currently amended) A reciprocating engine as claimed in Claim 43, wherein:
the a working chamber of the gases has a geometry revolving around the an axis of the cylinder:-
the stratification has a geometry revolving around the axis of the cylinder and created by the an orientation of the intake ports, and
the temperature of the a combustive charge increases between the a periphery and the axis so that the a self-ignition is propagated from the a centre towards the a periphery.
50. (currently amended) A reciprocating engine as claimed in Claim 49, wherein the a meridian profile of the combustion chamber is chosen so as to optimise optimize the a rate of release of energy by the a progressiveness of the isothermal surfaces of the a reactive load.
51. (new) A reciprocating engine as claimed in Claim 14,
wherein the maximum outlet section Sd max offered to the gases is formed by the two turbines which have fixed distributors mounted in parallel, and

wherein, in order to pass the turbines from the series configuration to the parallel configuration, the following manoeuvres are carried out simultaneously and with rapidity:

- total opening of an HP waste gate,
- total closing of an LP waste gate,
- putting the outlet of the HP turbine into communication with the outlet of the LP turbine.